

EXPERIMENTAL INVESTIGATION OF WEAR BEHAVIOUR OF A356-TiB₂ METAL MATRIX COMPOSITES

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ABSTRACT

Aluminium-Silicon (Al-Si) alloys have attractive physical and mechanical properties. They are light weight (app. 3x lighter than gray cast iron and steel), low cost of production (with sand casting technology), easy to machine and have satisfactory mechanical properties with good recycling possibilities (up to 95 %). Nevertheless, one of the major drawbacks of these alloys is their low wear resistance. In order to improve its wear characteristic many Particle reinforced Aluminium Matrix Composites (PAMCs) were developed using SiC, TiC, B₄C, TiB₂, Gr, MoS₂ and fly ash as reinforcement particles by different methods (Stir casting, Compo casting, Powder Metallurgy, in-situ method using salts and spray deposition) and their wear characteristics were also studied But there is no research work done on wear characteristics of semisolid processed PAMCs. So a MMC of aluminium A356 reinforced with 5%TiB₂ was developed by semi solid process and its dry sliding wear characteristic were studied using pin on disc machine with disc material of EN31 steel (55-60 HRC) under the condition at sliding velocity varies from 1m/s to 3m/s and applied load varies from 10N to 30N at constant sliding distance 3000m. A comparative study was done between A356 alloy, A356-5%TiB₂ in-situ composite and Semisolid processed alloy, composite it was found that semisolid processed alloy and composite shows more wear than commercial alloy and in-situ composite.

KEYWORDS: In-Situ MMCs Al, Thixo Forming, Dry Sliding Wear & Taguchi Techniques

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INTRODUCTION

MMCs offer the following advantages: Major weight savings due to higher strength-to-weight ratio Exceptional dimensional stability, higher elevated temperature stability, i.e., creep resistance significantly improved cyclic fatigue characteristics. With respect to PMCs, MMCs offer these distinct advantages like Higher strength and stiffness, Higher service temperatures, Higher electrical conductivity, Higher thermal conductivity, Better transverse properties Improved joining characteristics, Radiation survivability, Little or no contamination. Wear is the most commonly encountered industrial problems leading to the replacement of components and assemblies in engineering. [1]

Wear is due to following mechanism as Abrasive, Adhesive, Erosion, Fretting and Chemical in industries wear is mainly due to abrasive upto 55% and Adhesive upto 15% [2]. Aluminium alloys are widely used for commercial application in the transportation, construction and similarly Engineering industries. Nowadays, main focus is given to aluminium as matrix material because of its unique combination of good corrosion resistance, low electrical resistance and it possesses excellent mechanical properties in addition to good corrosion resistance due to

which the alloy finds extensive application in Naval vessels manufacturing [3]. The wear resistance of aluminium alloys can be further improved by means of addition of reinforcement either by *ex-situ* or *in-situ* [4]. Both the hypoeutectic and hypereutectic Al-Si alloys have been in use for the tribological components of internal combustion engines in dry and lubricated contacts for long time. Wear rate decrease and load carrying capacity increase with increasing silicon content [5]. The wear rate of hypoeutectic Al-Si alloy is less than the wear rate of hypereutectic alloy [5][6].

Wear rate of A356-SiC_p decreases with increase in SiC_p on Pin on Disc experiment at load 192N, sliding speed 1 to 5m/s and sliding distance 15 Km [7]. The eutectic alloys shows the lower wear rate compared with all the alloys in Al-Si alloy system and the wear is mild when applied load is less than 35N and sliding speed 5.8m/s in Pin on Disc experiment [8]. Delaminative wear, abrasive wear and oxidative wear was observed in Al-7Si alloy [9]. The behaviour of aluminium reinforced with TiC, TiB₂, B₄C, SiC were synthesized and found that TiB₂ showed better mechanical property than other reinforcement [10]. Mechanical properties of A356 are improved by compo casting than in stir casting [11]. The *in-situ* techniques to fabricate aluminium based composite has improved the adhesion at interface and its mechanical properties [12]. The presence of TiB₂ greater than 2.5% in T6 treated A356 increase coefficient of friction at sliding speed 1m/s and 1800m of sliding distance for varying loads (19.6-78.4 N) in Pin on Disc experiment not varying the sliding velocity [13]. Devis et.al reviewed the wear behaviour of Al-Si alloys and other Al-based composite and suggested the effect of *in-situ* TiB₂, TiC and SiO₂ particles towards the wear behaviour needs further investigation [4]. Thixoformable alloys should have solidification interval range between 50-100°C, Temperature sensitivity at 0.4 fraction liquid is around 0.03/°C [14].

The present paper reports the dry sliding wear behaviour A356-TiB₂ MMCs synthesised by an semisolid processing technique thixoforming, which is used to manufacture near net shape components.

FABRICATION WORK

Fabrication Process

The A356 – 5% TiB₂ Composite was prepared by *in-situ* process using K₂TiF₄ and KBF₄ salts. The synthesis of composite is based on work done in [13]. The composite was prepared by regular stirring the mixture at 10 minutes intervals for 60 minutes in electric resistant furnace then the melt is poured into moulds and allowed to solidify. The semisolid processed composite is made by thixoforming process where the *in-situ* composite is reheated to 593°C and hold for 40 min to obtain non-dendrite structure then this reheated composite is poured into high pressure die for forming process at semisolid state. Semisolid processed A356 alloy is also prepared by same process.

Material Properties

The chemical composition of ascast A356 alloy is shown in Table 1

Table 1: Chemical Composition of A356 Alloy

Alloying Elements	Si	Fe	Mn	Mg	Ti	Al
Percentage (%)	7.01	0.406	0.0430	0.760	0.0610	91.4%

The micro Vickers hardness of Alloy and composite are obtained at 200g load for dwell time of 10s, hardness value are shown in Table 3 which shows there is increase in hardness value between ascast and thixoformed alloy and composite. The reason is due to formation of non-dendrite structure which is absent in alloy and *in-situ* composite which is shown in Figure 1. The density of the alloy and composite are measured by Archimedes principle the value of densities are shown in Table 2

Table 2: Hardness and Density of Materials

S.no	Materials	Micro Hardness (VHN)	Density (g/cm ³)
1	A356 alloy	71	2.649
2	THIXOFORMED A356 alloy	76.3	2.698
3	A356-5%TiB ₂	81	2.848
5	THIXOFORMED A356-5%TiB ₂	103	2.845

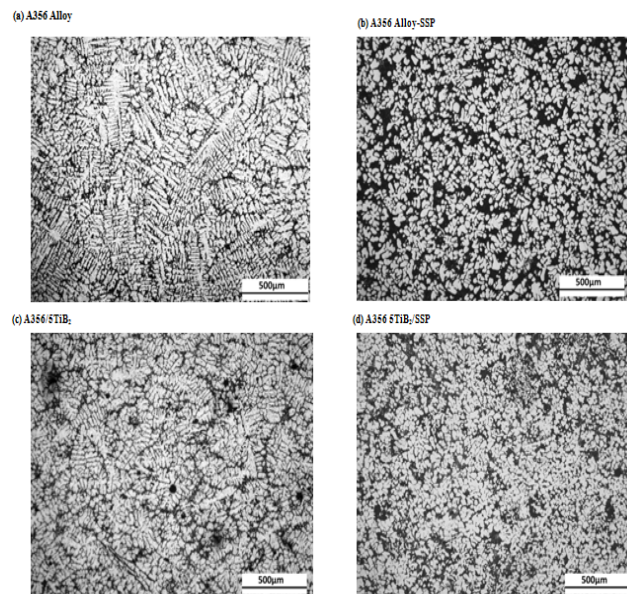


Figure 1: Optical Micro Structure of Alloy (a,b) and Composite(c,d)

There is slight increase in density in range of (0.005-0.050) for thixoformed composite and alloy.

Experimental Details

Pin on Disc machine is used to characterise the dry sliding wear behavior of the materials. Dry sliding wear test were conducted according to ASTM standard G99-04a. A cylindrical pin of dia 8mm and height 25mm is prepared for A356 alloy, *in-situ* A356-5%TiB₂, thixoformed A356 alloy and thixoformed A356-5%TiB₂ composite for wear test. The disc material is En31 steel (55-60 HRC). Trial experiment was carried out in A356 alloy at sliding velocity 5m/s, sliding load 50 N and sliding distance 3000m, and it was found that A356 alloy undergo severe adhesive wear called Galling as shown in Figure 2 (a) and Figure 2 (b) at 1000m on further continuation of experiment leads to seizure phenomenon. So, the significant parameters which affect wear property are Load and Sliding Velocity

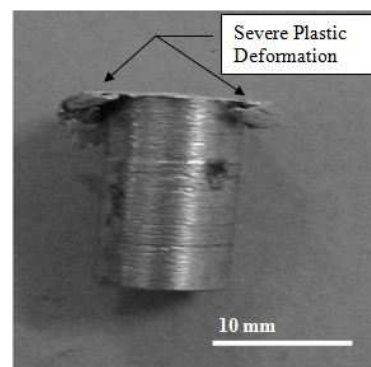


Figure 2(a): Galling in Pin

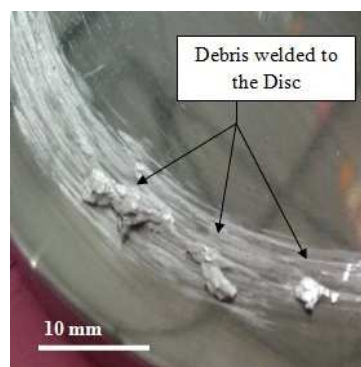


Figure 2 (b): Galling in Disc

Taguchi L9 orthogonal array is used to characterise the dry sliding wear behaviour of the materials where sliding velocity and load were taken as significant factors which vary from 1m/s to 3m/s and 10N to 30N respectively, as shown in Table 3.

Table 3: L9 Orthogonal Array

S.no	Sliding Velocity (m/s)	Load (N)
1	1	10
2	1	20
3	1	30
4	2	10
5	2	20
6	2	30
7	3	10
8	3	20
9	3	30

RESULTS

Wear Test

The effect of load and sliding velocity on wear rate is shown in Figure 3 which shows that wear rate of *in-situ* A356-5%TiB₂ is lesser than A356 alloy and the wear rate of thixoformed A356 alloy and thixoformed composite has greater wear rate than commercial A356 alloy, whereas increase in velocity decreases the wear rate. The effect of load on Coefficient of friction is shown in Figure 4(a) which shows that all four materials have average coefficient of friction ranges from (3 to 5) even on addition of TiB₂ particles.

The decrease in wear rate in *in-situ* composite than alloy is due to presence of secondary phase such as Si and TiB₂ as shown in figure 5(a) which restricts the flow of metal during sliding [14]. Increase in wear rate in thixoformed A356 alloy is due to breakage of Silicon needles, which tends to increase the ductility of the material which is shown in figure 6(a). Wear rate of all four materials shows that increase in load will increase the wear rate but increase in velocity decreases the wear rate, which is due to decrease in contact time between pin and disk to form micro welds on the disc surface, if the velocity is low micro welds will form which restricts the sliding movement of pin at contact surface which leads to removal of material and formation of grooves on pin. [14]

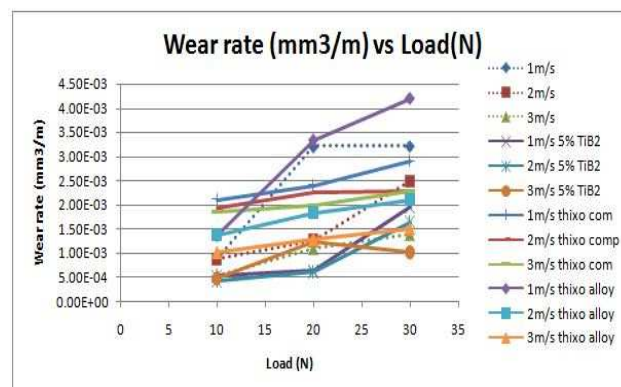


Figure 3: Wear Rate vs. Load

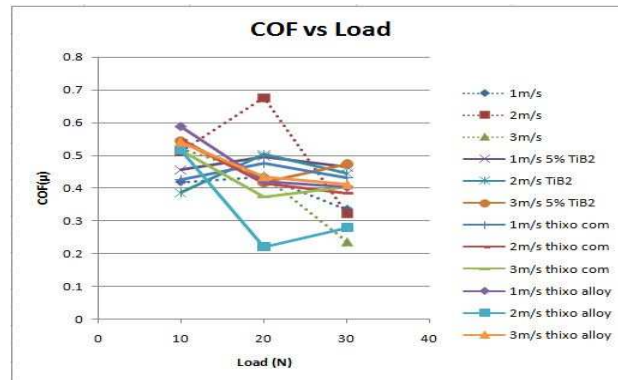


Figure 4 (b): COF vs. Load

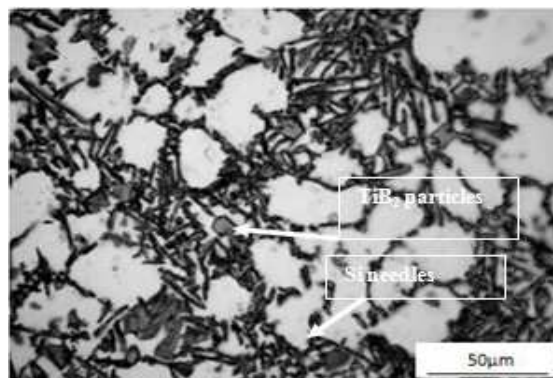


Figure 5 (a): Optical Microstructure of *in-situ* A356-5%TiB₂

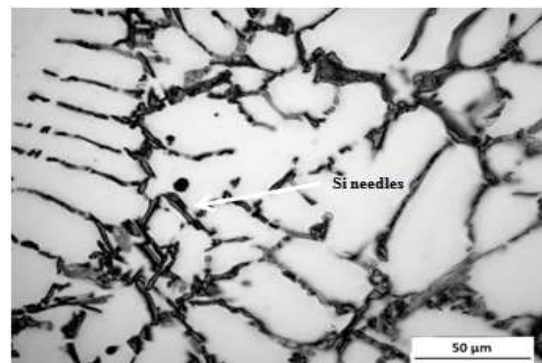


Figure 5 (b): Optical Microstructure of A356 Alloy

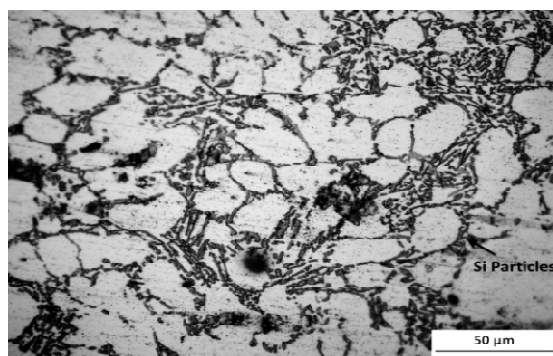


Figure 6 (a): Optical Microstructure of Thixoformed A356 Alloy

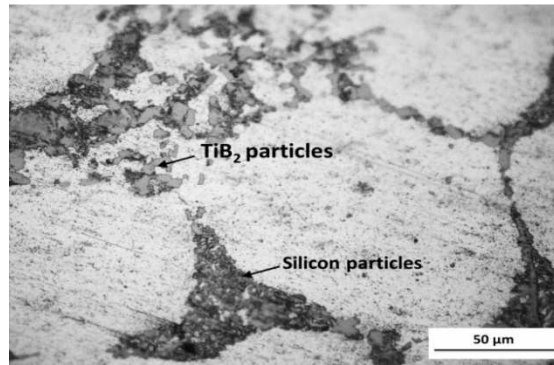


Figure 6 (b): Optical Microstructure of Thixoformed A356-5%TiB₂

From Figure 5(a),(b) and Figure 6 (a),(b) we can see that the size of silicon needles get reduced which is smaller in Semisolid processed alloy and composite because of high pressure used in thixoforming. This breakage leads to increase the wear rate.

Mini Tab Results

Taguchi L9 orthogonal array is used to characterise the wear behavior of the all four materials. The wear rate and COF of four materials is shown in below Table 4

Table 4: Wear Rate and COF of Four Materials

S.no	Sliding Velocity (m/s)	Load (N)	A356 Alloy		A356-5%TiB ₂		THIXOFORMED A356 Alloy		THIXOFORMED A356-5%TiB ₂	
			Wear Rate (mm ³ /m)	COF (μ)	Wear Rate (mm ³ /m)	COF (μ)	Wear Rate (mm ³ /m)	COF (μ)	Wear Rate (mm ³ /m)	COF (μ)
1	1	10	8.92E-04	0.41950	5.27E-04	0.455500	1.36E-03	0.5870	2.11E-03	0.4260
2	1	20	3.21E-03	0.43525	6.32E-04	0.496750	3.34E-03	0.4200	2.40E-03	0.4760
3	1	30	3.22E-03	0.33466	1.95E-03	0.464160	4.20E-03	0.4030	2.91E-03	0.4311
4	2	10	8.79E-04	0.51200	4.21E-04	0.386600	1.38E-03	0.5155	1.94E-03	0.5470
5	2	20	1.26E-03	0.67500	6.20E-04	0.503250	1.84E-03	0.2207	2.26E-03	0.4145
6	2	30	2.49E-03	0.32233	1.64E-03	0.444000	2.10E-03	0.2791	2.28E-03	0.3830
7	3	10	5.45E-04	0.52100	4.80E-04	0.542500	1.01E-03	0.5395	1.85E-03	0.5160
8	3	20	1.09E-03	0.43725	1.24E-03	0.417368	1.27E-03	0.4355	1.98E-03	0.3740
9	3	30	1.39E-03	0.23660	1.02E-03	0.473500	1.50E-03	0.4121	2.28E-03	0.4040

Wear rate and Coefficient of friction of A356 alloy is less at 3m/s and 30N as shown in Figure 7.

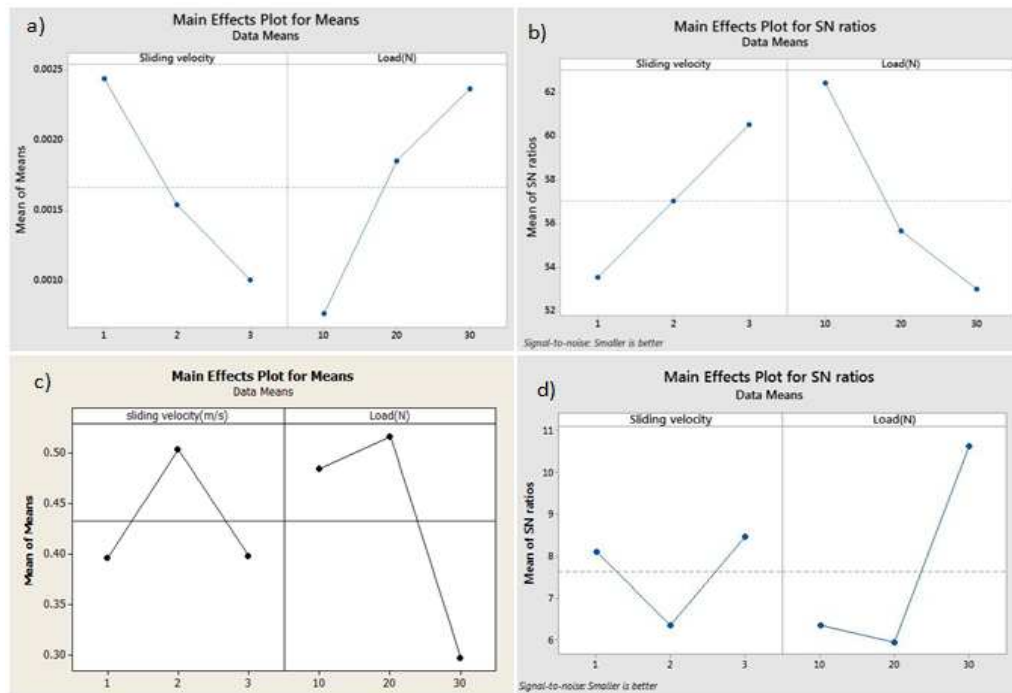


Figure 7: Mean Effects Plot for Mean a) Wear Rate, c) COF, Mean Effect Plots for S/N Ratio b) Wear Rate, d) COF

Wear rate and Coefficient of friction of *in-situ* A356-5%TiB₂ composite is low at 2m/s 10N and 30N as shown in Figure 8

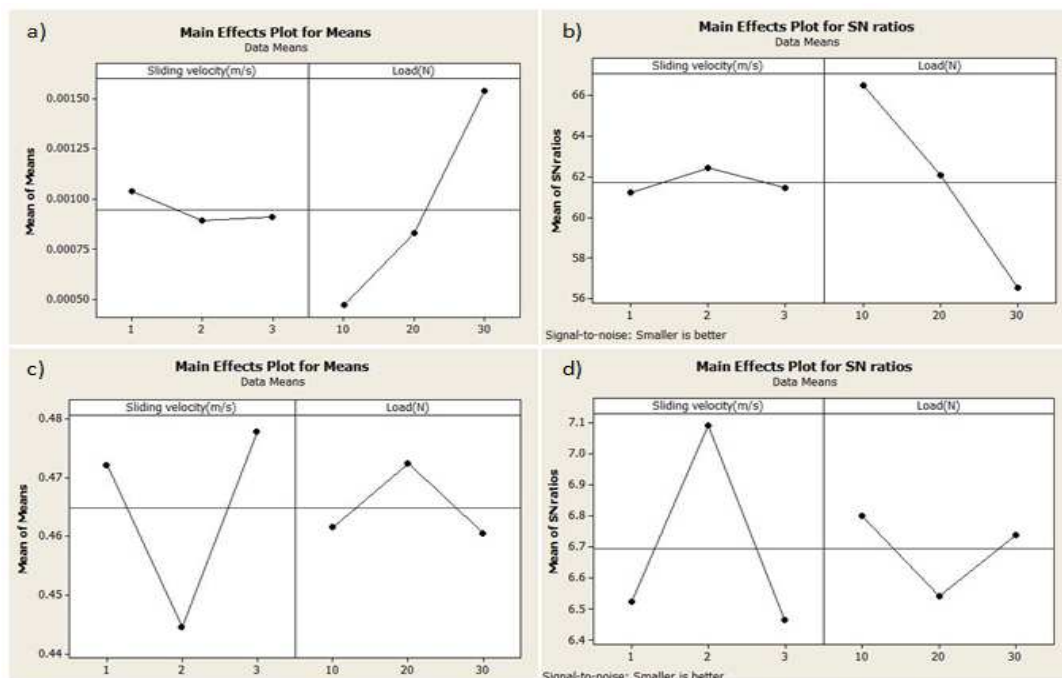


Figure 8: Mean Effect Plot for Mean a) Wear Rate, c) COF, Mean Effect Plot for S/N Ratio b) Wear Rate, d) COF

Wear rate and for thixoformed A356 alloy is less at 3m/s 10N and Coefficient of friction is minimum at 2m/s and 20N as shown in figure 9.

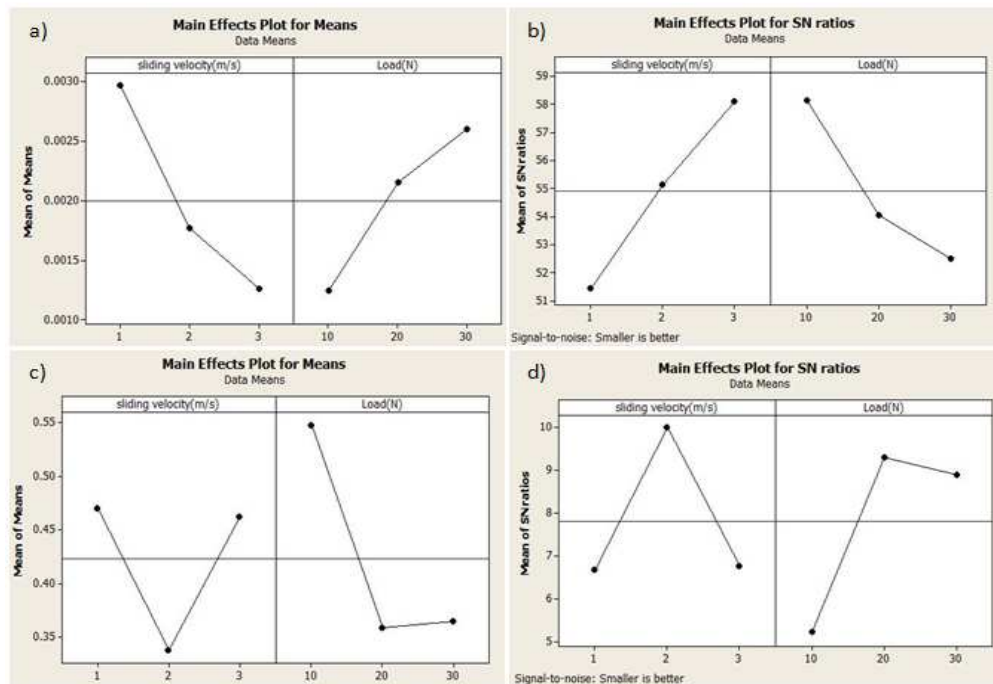


Figure 9: Mean Effect Plot for Mean a) Wear Rate, b) COF, Mean Effect Plot for S/N Ratio c) Wear Rate, d) COF

Wear rate and Coefficient of friction of thixoformed A356-5% TiB₂ is less at 3m/s 10N as shown in Figure 10

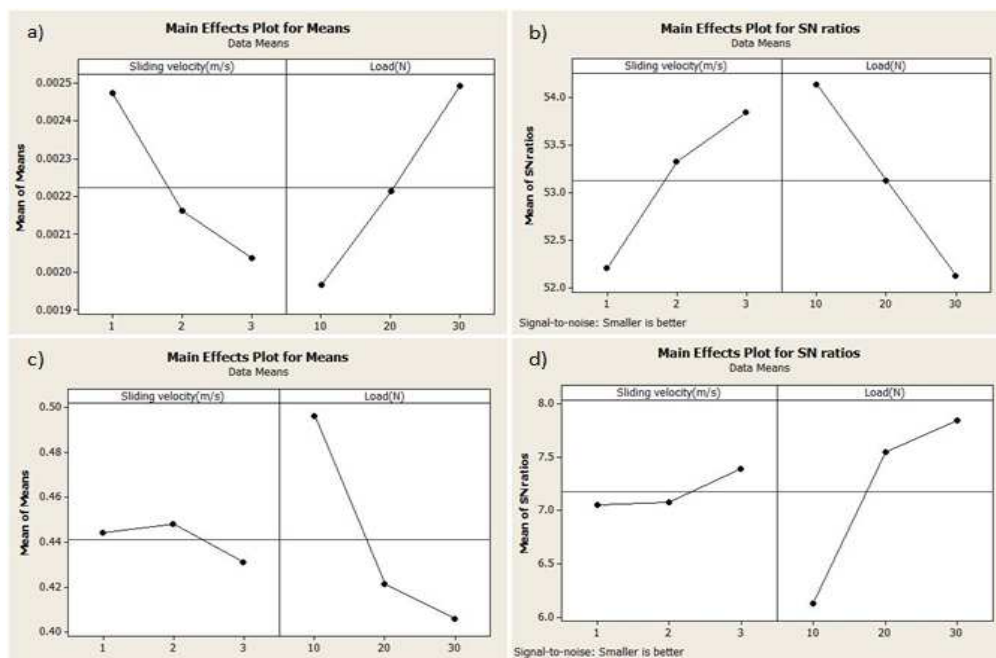


Figure 10: Mean Effect Plot for Mean a) Wear Rate, c) COF, Mean Effect Plot for S/N Ratio b) Wear Rate, d) COF

Thus, from Minitab Mean effect plot of Mean and S/N ratio of Wear rate and Coefficient of friction shows that wear rate is significantly affected by Load and Sliding Velocity.

CONCLUSIONS

- Wear rate of *in-situ* A356-5%TiB₂ is less than A356 alloy
- Wear rate is Maximum at 1m/s 30N and Minimum at 3m/s 10N
- Wear rate of thixoformed alloy and thixoformed Composite is greater than commercial alloy and *in-situ* composite
- Which is due to breakage of silicon needles which increase the ductility of the material
- Wear behavior of thixoformed alloy and thixoformed Composite is yet to interpret.
- Coefficient of friction doesn't change much, which is contradictory result from other research papers that require further interpretation

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